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Individuals with transtibial limb loss use interlimb force asymmetries to maintain multi-directional reactive balance control[☆]

Darren Bolger^a, Lena H. Ting^b, Andrew Sawers^{b,*}

^a School of Applied Physiology, Georgia Institute of Technology, 555 14th Street NW, Atlanta, GA 30318, United States

^b Wallace H. Coulter Department of Biomedical Engineering, Emory University and Georgia Institute of Technology, 313 Ferst Drive NE, Atlanta, GA 30332-0535, United States

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ABSTRACT

Background: Deficits in balance control are one of the most common and serious mobility challenges facing individuals with lower limb loss. Yet, dynamic postural balance control among individuals with lower limb loss remains poorly understood. Here we examined the kinematics and kinetics of dynamic balance in individuals with unilateral transtibial limb loss.

Methods: Five individuals with unilateral transtibial limb loss, and five age- and gender-matched controls completed a series of randomly applied multi-directional support surface translations. Whole-body metrics, e.g. peak center-of-mass displacement and net center-of-pressure displacement were compared across cohorts. Stability margin was computed as the difference between peak center-of-pressure and center-of-mass displacement. Additionally, center-of-pressure and ground reaction force magnitude and direction were compared between the prosthetic, intact, and control legs.

Findings: Peak center-of-mass displacement and stability margin did not differ between individuals with transtibial limb loss and controls for all perturbation directions except those loading only the prosthetic leg; in such cases the stability margin was actually larger than controls. Despite similar center-of-mass displacement, greater center-of-pressure displacement was observed in the intact leg during anterior–posterior perturbations, and under the prosthetic leg in medial–lateral perturbations. Further, in the prosthetic leg, ground reaction forces were smaller and spanned fewer directions.

Interpretation: Deficits in balance control among individuals with transtibial limb loss may be due to their inability to use their prosthetic leg to generate forces that are equal in magnitude and direction to those of unimpaired adults. Targeting this force-generating deficit through technological or rehabilitation innovations may improve balance control.

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1. Introduction

One of the most commonly cited functional mobility limitations facing individuals with lower limb loss (LLL) is a deficit in balance control (Jayakaran et al., 2012). Over half of community-living individuals with LLL report having fallen in the past year and 49.2% report a fear of falling (Miller et al., 2001). Ülger et al. (2010) found that 80% of geriatric amputees had fallen within the past year, with 64% falling more than once (Ülger et al., 2010). These impairments in balance control carry an immense cost to an individual's functional mobility at home and in the community (McWhinnie et al., 1994; van Velzen et al., 2006), lowering

their health-related quality of life (Pezzin et al., 2000). With LLL affecting more than 1.6 million individuals living in the United States, and forecast to increase to more than 3.6 million individuals by the year 2050 (Ziegler-Graham et al., 2008), the impact of balance impairments will continue to exact an increasing toll on the healthcare system. Although falling is clearly a common and serious problem among individuals with LLL (Pauley et al., 2006), very little is known regarding the challenges and mechanisms underlying deficits in balance control among individuals with LLL (Curtze et al., 2010).

To date, research investigating postural balance control in individuals with LLL has generally been limited to unperturbed standing (Jayakaran et al., 2012; Ku et al., 2014). These posturography studies have revealed increases in measures of postural sway including center of pressure velocity and displacement compared to age-matched controls (Buckley et al., 2002; Fernie and Holliday, 1978; Hermodsson et al., 1994; Isakov et al., 1992; Kolarova et al., 2013; Rougier and Bergeau, 2009). These differences in postural sway are influenced by

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* Corresponding author at: Department of Biomedical Engineering, Emory University and Georgia Institute of Technology, 313 Ferst Drive NE, U.A. Whitaker Bldg. 3111, Atlanta, GA 30332, United States.

E-mail address: ltting@emory.edu (A. Sawers).

age (Hermodsson et al., 1994; Vittas et al., 1986), cause of limb loss (Hermodsson et al., 1994), residual limb length (Lenka and Tiberwala, 2010), level of limb loss (Ferne and Holliday, 1978; Rougier and Bergeau, 2009), and time since limb loss (Mayer et al., 2011), but not prosthetic alignment (Isakov et al., 1994; Kolarova et al., 2013). Additionally, the intact leg may contribute substantially more to maintaining static postural stability than the prosthetic leg (Hlavackova et al., 2011).

In contrast to unperturbed standing balance, dynamic postural balance in response to internal or external perturbations has received much less attention among individuals with LLL, despite offering several advantages to other means of balance assessment (Visser et al., 2008). Aruin et al. (1997) studied anticipatory postural adjustments among a cohort of individuals with unilateral transtibial limb loss (TLL) in response to rapid arm raises. They found that individuals with TLL exhibited asymmetry in anticipatory changes of background muscle activity. These responses were much larger on the intact side of the body, and frequently absent on the side affected by limb loss (Arui et al., 1997). In response to external perturbations, individuals with unilateral TLL exhibit delayed muscle responses in both the intact and prosthetic leg (Rusaw et al., 2013), as well as greater reliance on the intact versus prosthetic leg to generate corrective responses (i.e. CoP displacement, ankle torque) (Curtze et al., 2012; Nederhand et al., 2012; Vrieling et al., 2008).

In these prior studies, perturbations were often limited to the sagittal plane (Curtze et al., 2010; Nederhand et al., 2012; Rusaw et al., 2013; Vrieling et al., 2008). Sagittal plane perturbations load both legs, allowing participants to compensate for sensorimotor impairment in one leg by using the contralateral leg more. Conversely, medial–lateral perturbations do not allow contralateral leg compensation, providing a direct assessment of each leg's capabilities. Medial–lateral balance control is also known to present greater fall risk (Maki et al., 1994; Topper et al., 1993), impose greater processing demands on the central nervous system (Carpenter et al., 1999), and be particularly challenging to individuals with LLL (Arifin et al., 2014). Furthermore, stance width (Vrieling et al., 2008), perturbation parameters (Nederhand et al., 2012), and cause of limb loss (Curtze et al., 2010, 2012; Nederhand et al., 2012; Vrieling et al., 2008), features known to influence postural responses (Henry et al., 2001; Hermodsson et al., 1994; Oude Nijhuis et al., 2014), were not standardized across subjects in previous studies. Additionally, several of the studies examining dynamic postural balance responses among individuals with LLL have used continuous (Vrieling et al., 2008) or predictable perturbations (Curtze et al., 2010, 2012). Lastly, little has been reported regarding the ability of individuals with unilateral TLL to generate ground reaction forces of appropriate magnitude and direction in response to multi-directional perturbations.

Our objective was to study reactive postural balance responses to multi-directional support surface translations in individuals with unilateral TLL. We examined net center of pressure (CoP) and center of mass (CoM) displacement, as well as CoP displacement and ground reaction forces (GRF) in each leg. Reactive balance control was quantified using the stability margin, the difference between the peak net CoP and peak CoM displacement during a perturbation (Horak et al., 2005; Winter et al., 1996). The smaller the stability margin, the more likely the individual is to lose their balance (Horak et al., 2005). Based on reported deficits in balance control in individuals with lower limb loss (Miller et al., 2001; Ülger et al., 2010), we hypothesized that individuals with unilateral TLL would have a smaller stability margin compared to unimpaired age-matched controls. We further hypothesized that individuals with unilateral TLL would display greater asymmetries between legs in maintaining their stability margin.

2. Methods

2.1. Recruitment

Inclusion criteria for individuals with unilateral TLL included: age greater than 18 years, time since limb loss greater than one year, cause of limb loss non-dysvascular, at least 8 h of prosthesis wear per day, and self-reported ability to ambulate with variable cadence, equivalent to K3 Medicare functional mobility level (i.e. ability to walk at variable cadences). Exclusion criteria were medical conditions, assessed by self-report, which could result in impaired balance or sensory loss, including significant musculoskeletal, neurologic, or cardiopulmonary conditions. All participants with unilateral TLL used their own prosthesis. Institutional Review Boards of Georgia Tech and Emory University approved all protocols. Written informed consent was obtained from each participant prior to enrollment.

2.2. Experimental protocol

Responses to balance perturbations were studied using a series of ramp-and-hold support surface translations in 12 evenly distributed and randomly applied directions in the horizontal plane (0–330°, every 30°), (Fig. 1A) (Torres-Oviedo and Ting, 2007). Each perturbation totaled 9 cm in total displacement, 35 cm/s peak velocity and 0.5 g (~490 cm/s²) peak acceleration. Four perturbations were given in each direction, for a total of 48 perturbations. During perturbations, participants were instructed to cross their arms over their chest and maintain balance without stepping, if possible. If a stepping response was required, the trial was excluded and the perturbation direction was repeated. Only perturbations in the four cardinal directions were analyzed.

Stance width was standardized based on subject-specific anthropometrics. Specifically, the centers of the subject's heels were positioned such that stance width equaled their inter-ASIS distance, which approximates the distance between the hip joints (Winter et al., 1998). The prescribed stance width was maintained during the protocol by marking the position of the subject's feet on the platform. To accommodate the built-in prosthetic heel height and standardize footwear across subjects, all subjects wore a standard shoe with a 3/8" heel height.

2.3. Data collection

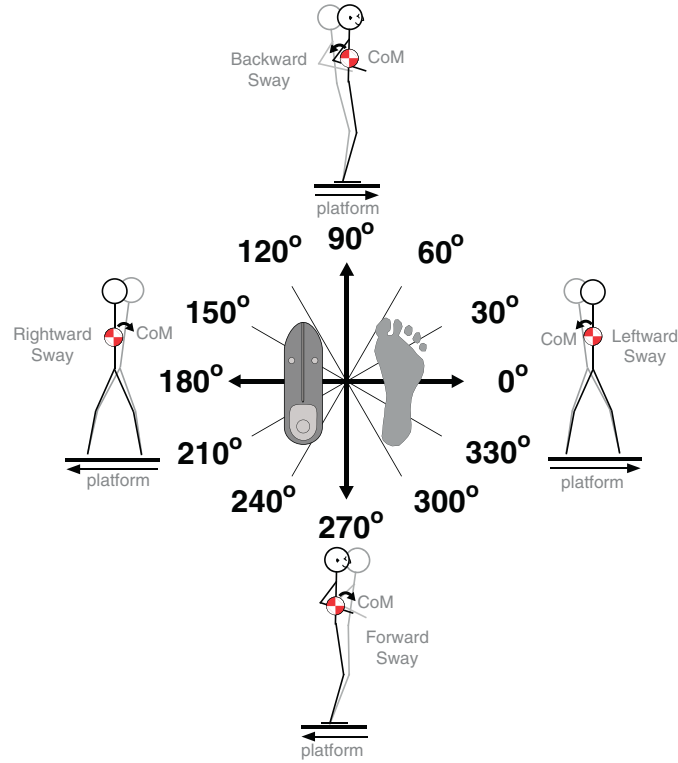
Twenty-five reflective markers were placed on participants' bony landmarks according to the Vicon Plug-in-Gait model. The position of markers on the prosthetic limb matched those of the sound limb. Three-dimensional marker coordinate data were collected at 120 Hz using an eight-camera motion capture system (Vicon, Centennial, CO) and synchronized with ground reaction force (GRF) data collected from force plates (AMTI, Watertown, MA) under each foot at 1080 Hz.

2.4. Data processing and analysis

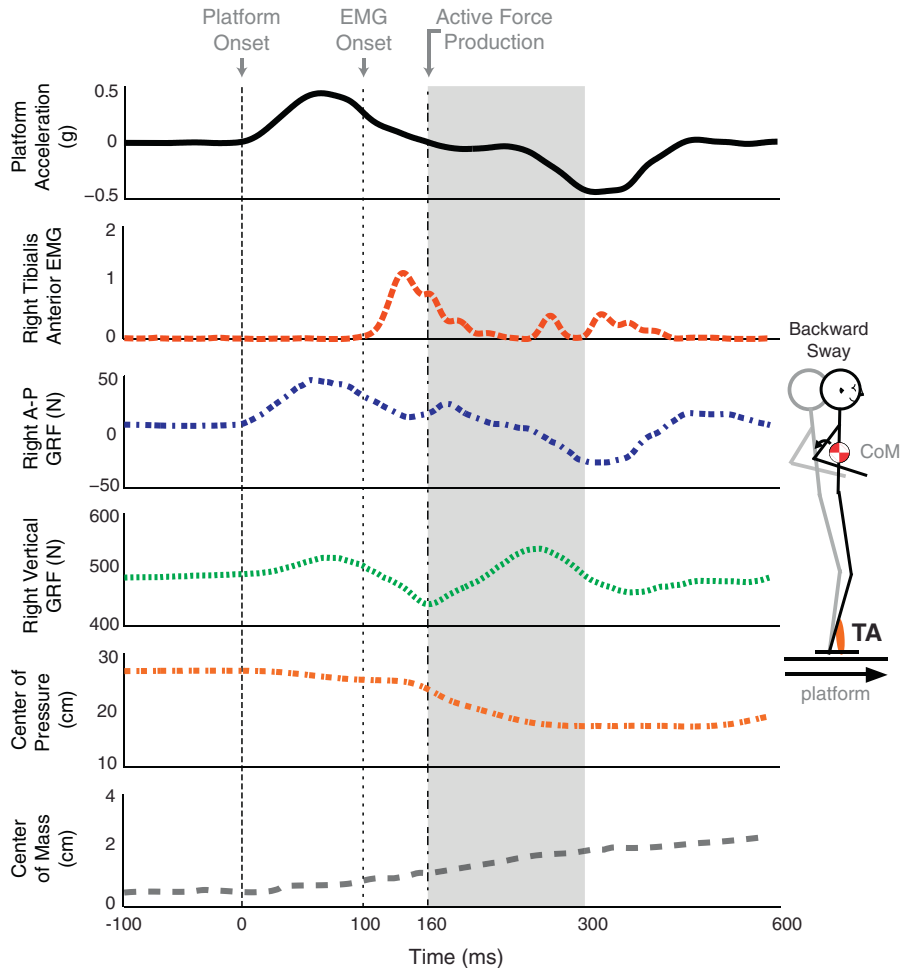
Marker coordinate data were filtered with a third-order Butterworth 30 Hz low-pass cut-off frequency and combined with participant-specific anthropometric data to calculate whole-body center of mass (CoM) position using the weighted sum approach. Differences in body segment parameters for the prosthetic foot were not taken into account. Ground reaction forces (GRF) were filtered with a third-order Butterworth 100 Hz low-pass cut-off frequency and used to calculate the CoP for individual force plates. The net CoP was calculated as the sum of the CoP from individual force plates multiplied by the percentage of body weight on each foot (Winter et al., 1993).

Fig. 1. Reactive postural response paradigm. A: Coordinate system for support surface translations in 12 evenly spaced directions along the horizontal plane with corresponding sway directions. B: Example of postural responses in the right leg to a forward translation of the support surface. Ground reaction forces, center of pressure, and center of mass displacement were examined during the active force production period, 160–300 ms after platform onset, of the automatic postural response (shaded area).

A. Coordinate system for support surface translations



B. Right leg response to forward perturbation



For each trial, whole-body reactive balance responses were quantified by calculating peak CoM and peak net CoP displacement from initial position, as well as the stability margin for each trial. Stability margin is the difference between peak CoP and CoM displacements during a perturbation (Horak et al., 2005; Winter et al., 1996). Peak net CoP, CoM and stability margin were analyzed from 160 to 300 ms following perturbation onset (Fig. 1B). This time period is referred to as the active force production period (Henry et al., 2001; Torres-Oviedo and Ting, 2007). 160 ms post-perturbation reflects the point in time when active force production begins, accounting for the excitation–contraction coupling time period. The ending time of 300 ms, which is prior to peak platform deceleration, was chosen to minimize the effect of the additional unwanted counterforce on the body caused by the deceleration of the platform.

Individual leg contributions to whole-body reactive balance responses were assessed for each perturbation direction by calculating leg-specific measures including: peak CoP displacement, the mean vertical, anterior–posterior (AP) and medial–lateral (ML) GRF magnitude, and the direction of the resultant horizontal GRF vector. The mean background GRFs were calculated during quiet stance, 250–50 ms prior to perturbation onset. The mean active GRF magnitude and the resultant horizontal force directions were computed over the first 60 ms time window of the active force production period (160–220 ms post-perturbation) as the change in force from background levels. All data was analyzed using custom MATLAB™ (MathWorks, Natick, MA) code.

2.5. Statistical analysis

To limit the number of statistical comparisons, four cardinal directions (forward, backward, right and left) of the 12 perturbation directions were subjected to statistical analysis. To determine the effect of group (TLL versus control) and sway direction (4 directions) on the dependent variables peak COM displacement, peak net CoP displacement, and stability margin, a 2-way mixed-design ANOVA (1-between group and 1-repeated measures factors) was performed for each variable. To determine the effect of leg (prosthetic, intact, matched control) and sway direction (4 directions) on leg-specific peak CoP displacement, a 2-way mixed-design ANOVA (1-between group and 1-repeated measures factors) was performed. Vertical, ML and AP GRFs were compared between leg conditions (prosthetic, intact, matched control) with a 1-way ANOVA. For background GRFs, the mean across all directions was compared. For active forces, the peak mean GRF across all directions was compared. Net and leg-specific active resultant horizontal GRF directions were plotted against sway direction for visual analysis. For all tests the level of significance was set at $\alpha = 0.05$. Post-hoc testing used the Sidak test. All statistical tests were conducted using SPSS (V.19; SPSS, Inc., Chicago IL).

3. Results

3.1. Participant demographics

Five males with unilateral TLL and five age- and gender-matched unimpaired adults were recruited to participate in the study (Table 1).

Table 1
Participant demographics.

Cohort		Height (m)	Mass (kg)	Age (years)	Gender	Etiology	Prosthetic foot type	Years since limb loss
TLL ^a (n = 5)	Mean (SD)	1.76 (0.25)	81.5 (14.8)	43.9 (13.7)	5 Male	Trauma (4) RSD ^b (1)	NA ESR ^c (4) Hydraulic ESR (1)	6.33 (6.88)
Controls (n = 5)	Mean (SD)	1.71 (0.33)	84.1 (16.0)	44.2 (15.5)	5 Male	N/A	N/A	N/A

^a TLL – transtibial limb loss.

^b RSD = Reflex Sympathetic Dystrophy.

^c NA ESR = non-articulated energy storage and response.

3.2. Differences in peak CoM, peak net CoP, and stability margin between groups

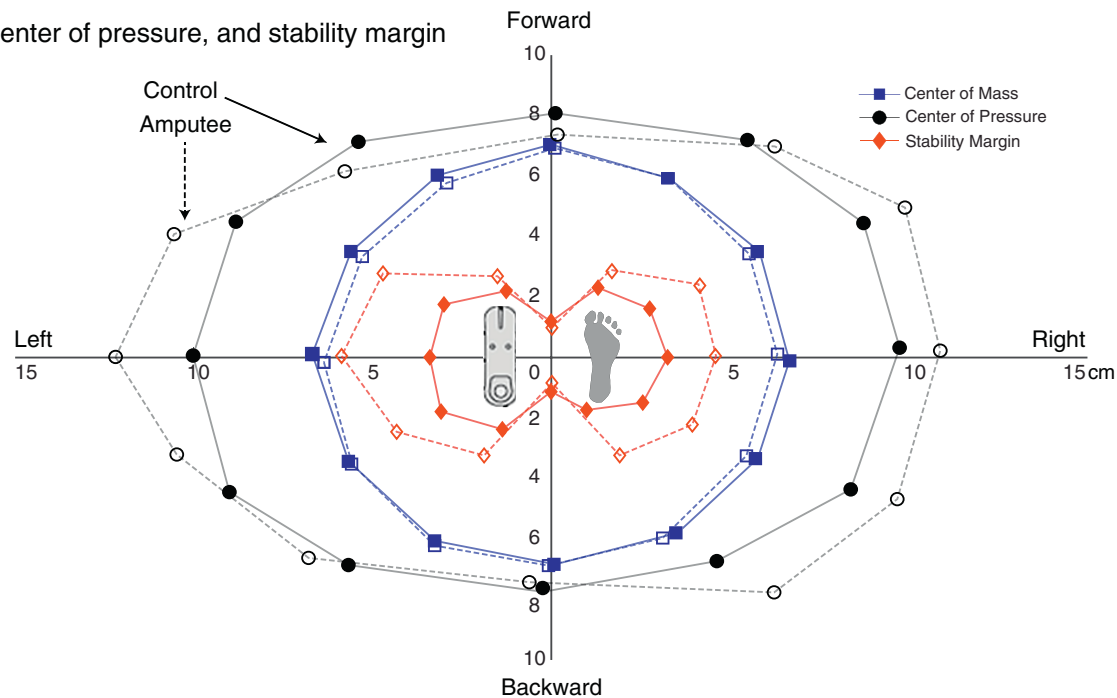
Although CoM displacement and net CoP magnitude did not differ between groups, we found directionally specific differences between individuals with TLL and controls in net CoP displacement and stability margin. Peak CoM displacement did not differ between groups (group effect: $P = 0.052$), across direction of sway (direction effect: $P = 0.16$), nor were there significant interaction effects (interaction: $P = 0.345$) (Fig. 2A–B). The magnitude of net CoP displacement did not differ between groups, while the stability margin did (group effect: net CoP $P = 0.062$; stability margin $P = 0.038$). Net CoP displacement and stability margin varied across directions (direction effect: net CoP $P < 0.001$; stability margin $P < 0.001$), with a significant interaction between group and direction (interaction: net CoP $P = 0.001$; stability margin $P = 0.003$). Specifically, individuals with TLL had significantly larger net CoP displacement ($P = 0.002$) and stability margin ($P = 0.002$) than controls when swaying towards and loading their prosthesis (leftward for controls) (Fig. 2A, C–D). Controls and individuals with TLL had significantly larger peak net CoP displacements during medial–lateral than anterior–posterior perturbations (controls $P < 0.029$; TLL $P < 0.001$) (Fig. 2A, C). These same directionally-sensitive differences in stability margin were only observed in individuals with TLL ($P < 0.003$), with controls demonstrating limited differences in stability margin across directions, leftward versus anterior–posterior sway ($P < 0.011$) (Fig. 2D).

3.3. Individual leg contributions to reactive balance responses (peak CoP, GRFs)

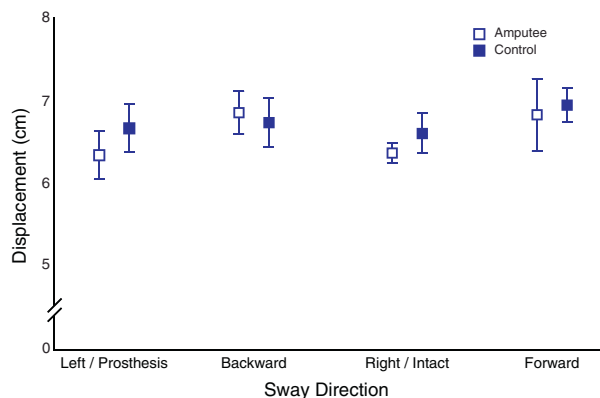
Individual leg force measurements revealed directionally specific differences in CoP displacement in the intact leg compared to the prosthetic and control legs. Peak CoP displacements for the right and left legs of controls were not significantly different ($P = 0.491$). Therefore the right leg was used for comparison to the peak CoP displacement of the prosthetic and intact legs of individuals with TLL. Leg-specific peak CoP displacement (Fig. 3) differed between legs (leg effect: $P = 0.004$), as well as by sway direction (sway direction effect: $P < 0.001$), with a significant interaction between leg and sway direction (interaction: $P < 0.001$). During forward sway, the intact leg of individuals with TLL had a significantly larger peak CoP displacement than the prosthetic leg ($P < 0.001$) or the control leg ($P = 0.002$). The control leg also had a significantly larger peak CoP displacement than the prosthetic leg ($P < 0.001$) (Fig. 3). During lateral sway (towards the prosthesis), the prosthetic leg of individuals with TLL had larger peak CoP displacement than the control leg ($P = 0.006$). Additionally, peak CoP displacement under the intact and prosthetic leg of individuals with TLL was significantly different across all sway directions (intact leg: $P < 0.001$, prosthetic leg: $P < 0.001$), while the peak CoP displacement among controls was only found to be significantly different between medial–lateral and anterior–posterior sway directions ($P < 0.001$).

Differences in force magnitude and direction were also observed between the prosthetic, intact and control legs. There were no significant differences in the mean background forces or the peak active forces between the left and right legs of control subjects ($P > 0.05$). The mean ML, AP, and vertical background forces were not significantly different

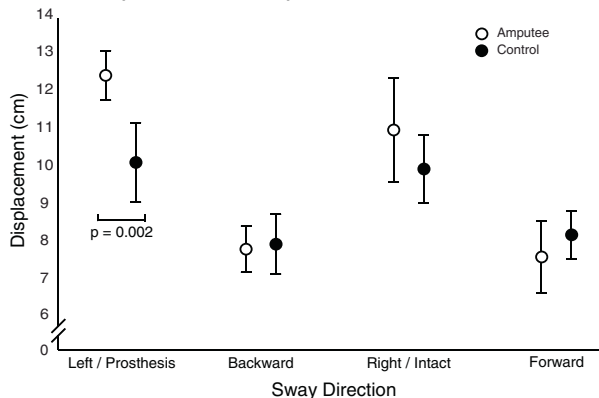
A. Center of mass, center of pressure, and stability margin



B. Peak center of mass



C. Net peak center of pressure



D. Stability margin

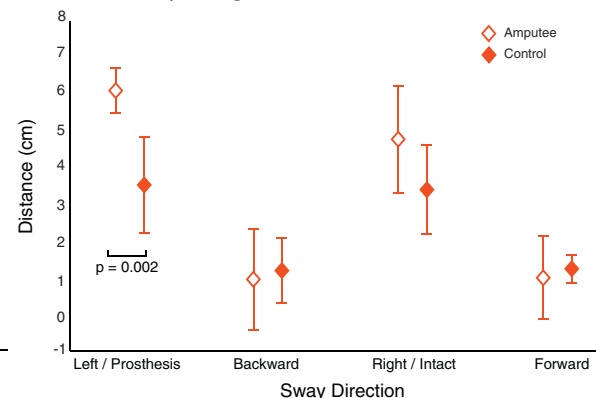


Fig. 2. Whole-body reactive balance responses to multi-directional support surface translations. A: Peak center of mass displacement (blue squares), peak net center of pressure excursion (black circles), and stability margin (red diamonds) averaged across subjects (transibial amputees: unfilled; controls: filled) for all 12 sway directions. B: Peak center of mass displacement (mean \pm 1SD) across the four cardinal directions for transibial amputees (unfilled) and controls (filled). There was no significant difference in the magnitude of whole-body displacement between individuals with limb loss and controls, or across directions within either cohort. C: Peak net center of pressure excursion (mean \pm 1SD) across the four cardinal directions for individuals with transibial limb loss (unfilled) and controls (filled). Individuals with transibial limb loss had significantly larger net center of pressure excursion in response to lateral sway that loaded the prosthetic leg ($P = 0.002$) than controls. D: Stability margin (mean \pm 1SD) across the four cardinal directions for individuals with transibial limb loss (unfilled) and controls (filled). Individuals with transibial limb loss had a significantly larger stability margin during lateral sway that loaded the prosthetic leg ($P = 0.002$) than controls.

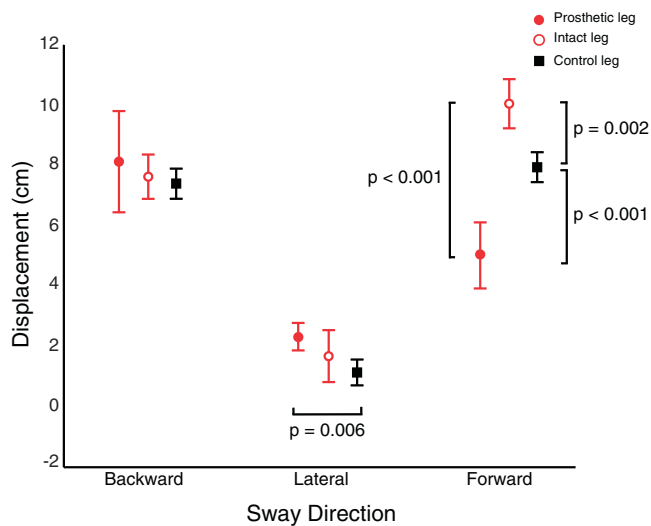


Fig. 3. Leg specific peak center of pressure excursion (mean \pm 1SD) for the prosthetic (filled circle), intact (unfilled circle), and control (filled square) legs. Peak center of pressure excursion on the intact leg of individuals with transtibial limb loss was significantly greater than that of the prosthetic ($P < 0.001$) and control ($P = 0.002$) legs during forward sway. Additionally, peak center of pressure excursion during lateral sway towards the prosthetic leg was significantly larger than in controls ($P = 0.006$) when the comparable leg was loaded.

between the prosthetic, intact or control legs ($P > 0.05$) (Fig. 4). Neither the ML ($P = 0.891$), nor the vertical ($P = 0.635$) peak active forces were significantly different between the prosthetic, intact or control legs; only the AP peak active force was significantly different between leg conditions (leg effect: $P = 0.002$). Specifically, the intact leg of individuals with TLL produced a significantly larger peak AP force than the prosthetic leg ($P = 0.002$) and the control leg ($P = 0.032$). While the prosthetic leg produced a smaller peak AP force than the control leg, this difference was not statistically significant ($P = 0.416$) (Fig. 4). Beyond the magnitude of the horizontal forces, inspection of Fig. 5 reveals that the direction of the resultant horizontal forces also differed between cohorts, specifically when comparing the prosthetic leg with that of the control leg (Fig. 5B).

4. Discussion

Individuals with TLL employ different interlimb kinetic strategies to achieve surprisingly similar dynamic balance performance compared to controls in most directions. Specifically, during lateral perturbations that loaded the prosthetic leg, similar CoM but greater net CoP displacement (Fig. 2A) was found, resulting in a higher, not lower stability margin in the direction considered the least stable. Differences in interlimb coordination of individual leg CoP and ground reaction forces were also observed across directions suggesting more reliance on the intact leg for balance. Limited directions of force were identified in the prosthetic leg compared to the intact and control legs, however it is unclear whether this reflects a compensatory strategy or a functional limitation related to the design of prostheses.

The exaggerated net CoP response that was observed among individuals with TLL may impose additional unintended balance challenges and result from a fear of falling and/or sensorimotor limitations of the prosthesis. The exaggerated net CoP response may have developed as a result of a history of falls. Repeated falls could create the desire to maintain a greater margin for error to reduce the likelihood of a loss of balance, particularly when using the prosthetic leg (Hof et al., 2007). Four of the five individuals with TLL in this study reported at least one fall in the past 12 months, suggesting that their control strategy for maintaining balance could have been influenced by their falls' history. Another explanation could be the inability to accurately perceive the

perturbation, or to generate appropriately scaled forces with the prosthetic leg. It is possible that the prosthetic leg was used passively as a strut rather than actively to generate forces. Regardless of its cause, this exaggerated response may impose unforeseen challenges to maintaining balance control. If individuals with unilateral TLL use motor responses that are larger than necessary, and that lie at the limits of their capabilities, this may constrain their ability to respond to continued or larger perturbation(s). If so, a disproportionate response may leave them with little in reserve to cope with continued or subsequent perturbations, ultimately resulting in a loss of balance and potential for serious injury. Testing this hypothesis would require identifying the maximal capacity of subjects during reactive balance, comparing it to responses across other perturbation magnitudes, and assessing whether the use of an exaggerated response across perturbation magnitudes does in fact limit their ability to respond effectively to continued perturbations. This would likely require an examination of stepping (Curtze et al., 2010, 2012; Mansfield et al., 2013; Mille et al., 2003; Rogers et al., 2003) and non-stepping responses.

The differences in balance between individuals with TLL was likely not due to their initial posture, but rather the execution of the motor response following a perturbation. While visually distinct, we found that the background forces were not significantly different between controls and individuals with TLL (Fig. 4), consistent with the results of Nederhand et al. (2012). This does not exclude the possibility that adjustment(s) to background posture or force patterns would not improve reactive balance among individuals with LLL (Anker et al., 2008; Genthon and Rougier, 2005).

Consistent with prior studies in perturbed (Curtze et al., 2012; Vrieling et al., 2008) and unperturbed standing (Nadollek et al., 2002; Quai et al., 2005), compensations in the intact leg were required to preserve anterior–posterior balance. If the individuals with TLL in our study had not increased the CoP displacement under their intact leg during forward sway (Fig. 3), the peak CoM displacement would have exceeded the net CoP response, resulting in a loss of balance. This asymmetric strategy was effective in maintaining a similar stability margin as controls (Fig. 2A, D), and was achievable due to the relatively high mobility level of the amputee subjects in this study. However, older adults with TLL, or those with additional co-morbidities such as neuropathy, may lack adequate contralateral sensorimotor function to effectively compensate for the reduced biomechanical contributions of the prosthetic leg to anterior–posterior balance. Additional research is required to determine how these compensations are affected by aging and additional impairment. The differences in interlimb contributions to balance also highlight the need for interventions and innovations in prosthetic technology to reduce the need for contralateral compensations.

Consistent with previous work (Nederhand et al., 2012; Vrieling et al., 2008), force-generating asymmetries between legs were observed in the anterior–posterior direction, with the intact leg exerting significantly greater peak AP forces than the prosthetic or control legs. Deficits in force magnitude were limited to the AP direction, as individuals with unilateral TLL are able to use their prosthetic leg to produce ML and vertical forces of equivalent magnitude to those of controls and their own intact leg (Fig. 4A, C, E). The large difference in the AP force magnitude may reflect limitations in the ability to actively generate plantarflexion torque with the prosthetic leg. Further, this exaggerated force response may characterize a preferred strategy used by individuals with TLL to simplify the control of reactive balance. If a single exaggerated yet safe response is consistently used, it may remove the need to scale the response according to the perturbation and/or need for contralateral compensation, thereby simplifying control.

Individuals with TLL demonstrated limited directions of force with their prosthetic leg, altering interlimb force coordination for directional control of the CoM. Individuals with unilateral TLL exerted active resultant horizontal GRFs with their prosthetic leg that clustered around the medial–lateral directions, while forces generated by control and intact legs were distributed across all directions in the horizontal plane

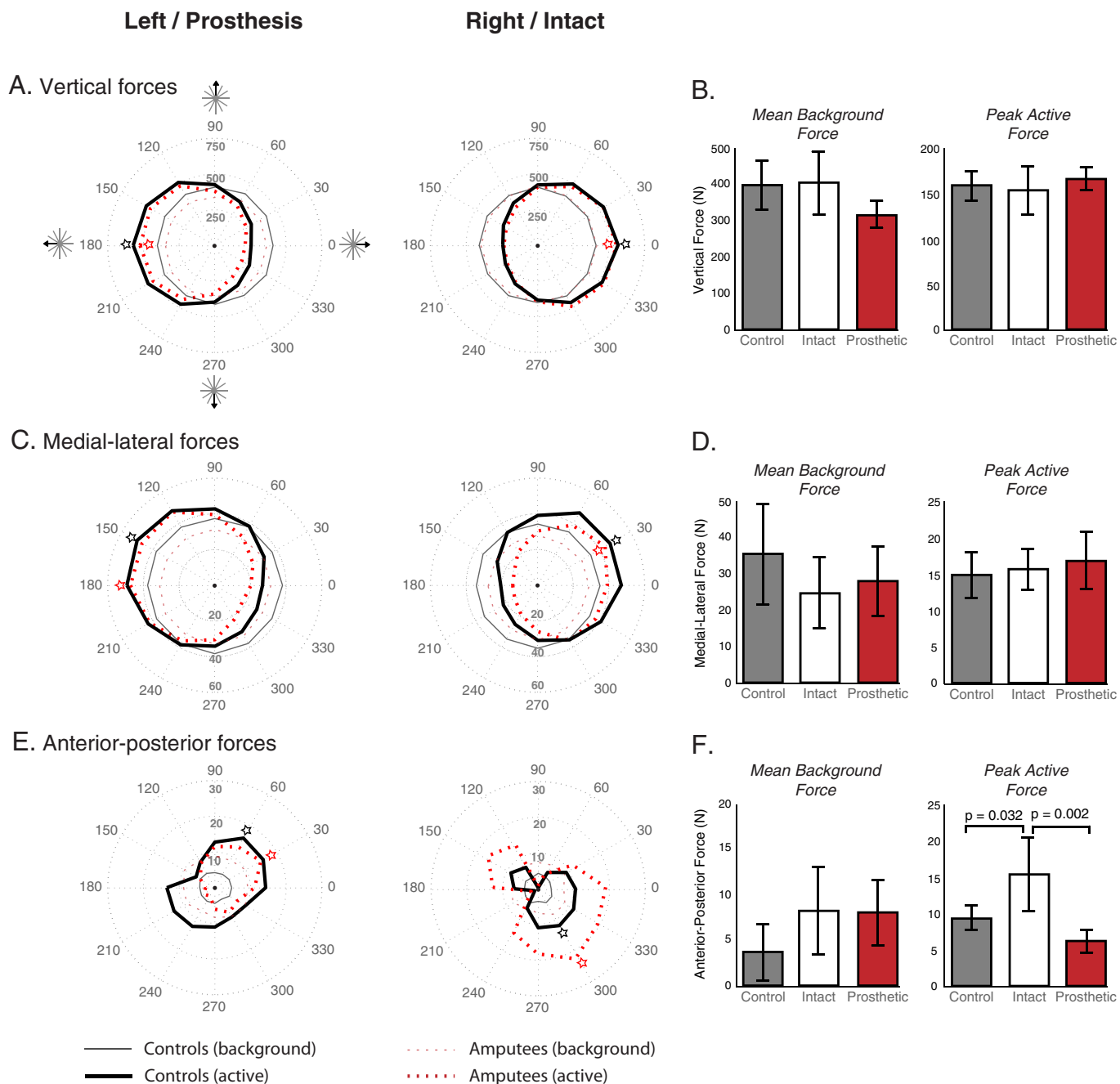


Fig. 4. Background and active period ground reaction forces. A, C, E: Polar plots for each leg depicting the mean background (thin lines) and active period (thick lines) vertical (A), medial-lateral (B), and anterior-posterior (C) ground reaction force for controls (solid black lines) and individuals with transtibial limb loss (dashed red lines) across each direction of sway. B, D, F: The mean background force (± 1 SD) and peak active force (± 1 SD) along the vertical (B), medial-lateral (D), and anterior-posterior (F) axes for the control (gray), intact (white) and prosthetic (red) legs. Polar plots reveal a non-significant difference in vertical (prosthetic vs. control leg), medial-lateral (prosthetic vs. control; intact vs. control), and anterior-posterior (prosthetic vs. control; intact vs. control) background forces. The patterns of active forces were largely comparable between controls and individuals with transtibial limb loss along the vertical and medial-lateral axes, with no significant differences in the peak active forces. The patterns of active forces were vastly different between cohorts along the anterior-posterior axis, with significant differences between the control and intact leg ($P = 0.032$), as well as the intact and prosthetic leg ($P = 0.002$). Peak active forces were generally exerted in the same direction by controls and individuals with transtibial limb loss (denoted by star).

(Fig. 5B–C). By restricting forces to a set of two direction-invariant vectors, the challenge of maintaining balance in response to horizontal plane perturbations may be simplified (Macpherson, 1988). Such a restriction of force direction has been observed previously for non-preferred stances in both humans (i.e. narrow stance) and animals (Henry et al., 2001; Macpherson, 1994). It is possible that the force constraint strategy simplifies the control of balance under novel, or challenging balance conditions. We only observed the constraint in the prosthetic leg suggesting that the intact leg regulates multi-directional

control of the CoM among individuals with unilateral TTLL. However, the medial-lateral force constraint may also be due to limitations in sagittal plane ankle range of motion or plantarflexion torque generation in the prosthetic ankle.

4.1. Study limitations

We studied only five individuals with TTLL, limited to those of traumatic etiology. Given the increasing age of the general population

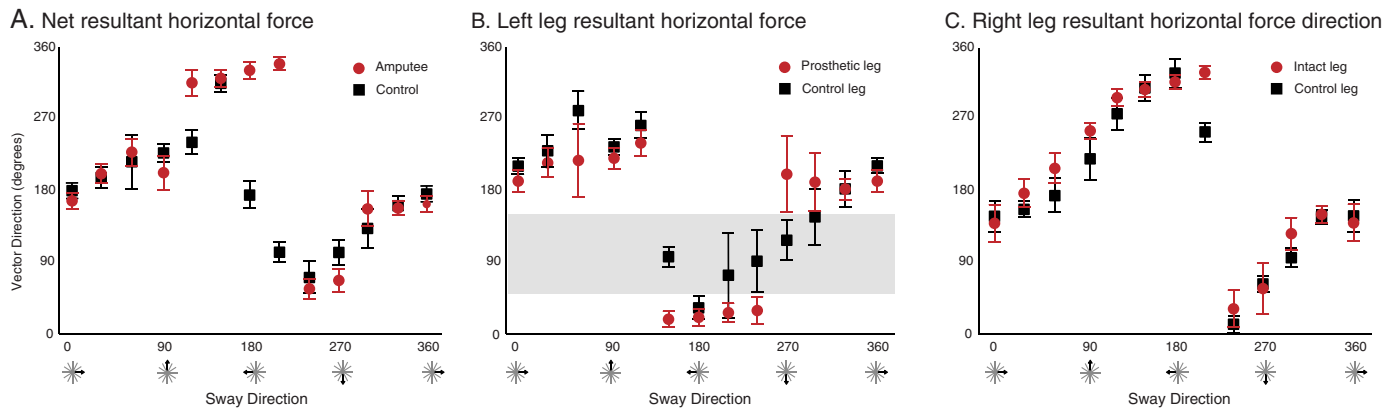


Fig. 5. Direction of resultant horizontal force vectors. A: Direction (mean \pm 1SD) of the net resultant horizontal force vectors for each of the 12 sway directions. The direction of the net resultant horizontal force vectors was similar between controls (black squares) and individuals with transtibial limb loss (red circles) across sway directions, the main exception being sway in the direction of the prosthesis (leftward). B: Direction (mean \pm 1SD) of the resultant horizontal force vector exerted by the prosthetic (red circles) and left leg of controls (black squares). Controls exerted forces across a wider range of directions than individuals with transtibial limb loss who tended to constrain the forces they exerted with their prosthetic leg to two principle directions, approximately 180 and 0°. Note that individuals with transtibial limb loss did not exert forces with their prosthetic leg across a range of directions, namely 45 to 160° (shaded area). C: Direction (mean \pm 1SD) of the resultant horizontal force vector exerted by the intact leg of individuals with transtibial limb loss (red circles) and right leg of controls (black squares). Note that the direction of the resultant horizontal force vectors was virtually equivalent across all sway directions.

(Wiener and Tilly, 2002), and the rising incidence of diabetes (Boyle et al., 2010), there is an unmistakable need to study individuals with dysvascular limb loss as well as older adults with lower limb loss. However, for this initial study the traumatic population was specifically selected to avoid additional confounds that may influence reactive balance control. Despite a limited sample size we were able to identify significant differences between cohorts. Nevertheless, a study including a larger cohort of subjects is certainly warranted to confirm these results. The perturbation parameters selected in this study were selected based upon previous work (Henry et al., 2001; Horak et al., 2005) and were sufficient to examine the initial active response period. However, the short time interval between peak platform acceleration and deceleration precluded us from looking at a longer time window. Here we examined whole-body kinematics and endpoint forces to describe differences in reactive postural balance control between individuals with unilateral TLL and unimpaired adults. An analysis of the muscle coordination patterns that underlie the differences in control strategies used to stabilize the same CoM displacement (Chvatal and Ting, 2013; Chvatal et al., 2011; Torres-Oviedo and Ting, 2007), may provide additional insight into their production and the design of interventions to improve balance control among individuals with LLL.

5. Conclusion

Surprisingly, we found that individuals with non-dysvascular unilateral TLL were equally capable of maintaining dynamic standing balance in response to external perturbations as age-matched unimpaired controls. Individuals with TLL used significantly different interlimb contributions to stabilize the same CoM displacement, revealing functional asymmetries in CoP and ground reaction forces between the prosthetic, intact and control legs. These functional asymmetries between legs suggest that individuals with unilateral TLL may be limited in their ability to exert forces with their prosthetic leg that are equal in magnitude and direction to those of unimpaired adults. These deficits in force production may underlie many of the postural and walking balance impairments attributed to individuals with lower limb loss.

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